

**WHAT IS CLAIMED IS:**

1. An estimating apparatus for a secondary cell, comprising:

5 a current detecting section that detects a current (I) charged into and discharged from the secondary cell;

a voltage detecting section that detects a terminal voltage (V) across the secondary cell;

10 a parameter estimating section that integrally estimates all parameters ( $\theta$ ) at one time in at least one of the following equations (1) and (2) with the measured current (I) and terminal voltage (V) inputted into an adaptive digital filter using a cell model described in a corresponding one of the following equations (1) and (2) whose parameters are estimated;

15 an open-circuit voltage calculating section that calculates an open-circuit voltage ( $V_o$ ) using the current (I), the terminal voltage (V), and the parameter estimated values ( $\theta$ );

20 an input enabling power estimating section that estimates an input enabling power ( $P_{in}$ ) of the secondary cell on the basis of the parameter estimated values ( $\theta$ ) and open-circuit voltage ( $V_o$ );  
25 and

30 an output enabling power estimating section that estimates an output enabling power ( $P_{out}$ ) of the secondary cell on the basis of the parameter estimated values and the open-circuit voltage ( $V_o$ ), the equation (1) being

$$V = \frac{B(s)}{A(s)} \cdot I + \frac{1}{C(s)} \cdot V_o \quad \dots (1), \text{ wherein}$$

$$A(s) = \sum_{k=0}^n a_k \cdot s^k, \quad B(s) = \sum_{k=0}^n b_k \cdot s^k, \quad C(s) = \sum_{k=0}^n c_k \cdot s^k, \quad s$$

denotes a Laplace transform operator,  $A(s)$ ,  $B(s)$ , and  $C(s)$  denote each poly-nominal of  $s$  ( $n$  denotes degrees),  $a_1 \neq 0$ ,  $b_1 \neq 0$ , and  $c_1 \neq 0$  and the equation

5 (2) being  $V = \frac{B(s)}{A(s)} \cdot I + \frac{1}{A(s)} \cdot V_0 \dots (2)$ , wherein

$$A(s) = \sum_{k=0}^n a_k \cdot s^k \quad \text{and} \quad B(s) = \sum_{k=0}^n b_k \cdot s^k.$$

2. An estimating apparatus for a secondary cell as claimed in claim 1, wherein the adaptive digital filter uses the cell model described in the equation 10 (1) and the parameter estimating section integrally estimates all of the parameters ( $\theta$ ) in the equation (1) at one time and wherein, in a case where the terminal voltage of the secondary cell immediately 15 before the secondary cell becomes a predetermined excessive charge is assumed to be a maximum enabling voltage ( $V_{max}$ ) and the terminal voltage of the secondary cell immediately before the secondary cell becomes a predetermined excessive discharge is assumed to be a minimum enabling voltage ( $V_{min}$ ), the 20 input enabling power estimating section estimates the input enabling power ( $P_{in}$ ) of the secondary cell on the basis of the parameter estimated values ( $\theta$ ), the open-circuit voltage ( $V_0$ ), and the maximum enabling voltage ( $V_{max}$ ) and the output enabling power estimating section estimates the output enabling power ( $P_{out}$ ) of the secondary cell on the basis of the parameter estimated values ( $\theta$ ), the open-circuit voltage ( $V_0$ ), and the minimum enabling voltage ( $V_{min}$ ).

3. An estimating apparatus for a secondary cell as  
claimed in claim 2, wherein the input enabling power  
estimating section calculates  $V_o/C(s)$  from the  
5 parameter estimated values and the open-circuit  
voltage ( $V_o$ ) and the input enabling power estimating  
section estimates the input enabling power ( $P_{in}$ ) of  
the secondary cell on the basis of one of the open-  
circuit voltage ( $V_o$ ) and the calculated ( $V_o/C(s)$ )  
10 whose value is nearer to the maximum enabling voltage  
( $V_{max}$ ), the parameter estimated values ( $\theta$ ), and the  
minimum enabling voltage ( $V_{min}$ ).

4. An estimating apparatus for a secondary cell as  
15 claimed in claim 2, wherein the output enabling power  
estimating section calculates  $V_o/C(s)$  from the  
parameter estimated values ( $\theta$ ) and the open-circuit  
voltage ( $V_o$ ) and the output enabling power estimating  
section estimates the output enabling power ( $P_{out}$ ) of  
20 the secondary cell on the basis of one of the open-  
circuit voltage ( $V_o$ ) and the calculated  $V_o/C(s)$  whose  
value is nearer to the minimum enabling voltage ( $V_{min}$ ),  
the parameter estimated values ( $\theta$ ), and the maximum  
output enabling voltage ( $V_{max}$ ).

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5. An estimating apparatus for a secondary cell  
as claimed in claim 2, wherein the input enabling  
power estimating section calculates  $V_o/C(s)$  from the  
parameter estimated values ( $\theta$ ) and the open-circuit  
30 voltage ( $V_o$ ) and estimates the input enabling power  
( $P_{in}$ ) of the secondary cell on the basis of one of  
the open-circuit voltage ( $V_o$ ) and the calculated  
 $V_o/C(s)$  whose value is nearer to the maximum enabling

voltage ( $V_{max}$ ), the parameter estimated values ( $\theta$ ), and the maximum enabling voltage ( $V_{max}$ ) and wherein the output enabling power estimating section estimates the output enabling power ( $P_{out}$ ) of the 5 secondary cell on the basis of one of the open-circuit voltage ( $V_o$ ) and the calculated  $V_o/C(s)$  whose value is nearer to the minimum enabling voltage ( $V_{min}$ ).

6. An estimating apparatus for a secondary cell 10 as claimed in claim 5, wherein the input enabling power estimating section estimates the input enabling power ( $P_{in}$ ) using the following equation:

$$\begin{aligned} P_{in} &= I_{in\_max} \cdot V_{max} \\ &= \frac{V_{max} - V_0}{e} \cdot V_{max} \end{aligned} \quad ]$$

, wherein  $I_{in\_max}$  denotes a maximum input current to 15 the secondary cell calculated from the following equation:  $V = K \cdot I + V_0$ , wherein  $e$  is substituted for  $K$ ,  $V_{max}$  is substituted into  $V$ ,  $I_{in\_max}$  is substituted for  $I$ , and  $V_o(k)$  is substituted for  $V_0$ ,  $V_o(k) = \Delta V_o(k) + V_{ini}$ , wherein  $V_o(k)$  is substituted 20 for  $\Delta V_o(k)$  and  $V_{ini}$  denotes an initial value of the terminal voltage when no current from the secondary cell is caused to flow, and  $e = K + h \cdot T_1 \doteq K$ , wherein  $K$  denotes one of the parameter estimated values ( $\theta$ ) which corresponds to an internal resistance of the 25 secondary cell, when the calculated open-circuit voltage  $V_o(k)$  at a time point of  $k$  is equal to or higher than an apparent open-circuit voltage  $V'_o(k)$  and estimates the input enabling power ( $P_{in}$ ) using the following equation:

$$\left. \begin{aligned} P_{in} &= I_{in\_max} \cdot V_{max} \\ &= \frac{V_{max} - V_o}{e} \cdot V_{max} \\ &= \frac{V_{max} - \frac{V_o}{b \cdot s + 1}}{e} \cdot V_{max} \end{aligned} \right]$$

, wherein  $b = T_3 + T_1 \approx T_3$  and  $T_1$  and  $T_3$  denotes time constants, when the calculated open-circuit voltage  $V_o(k)$  at the time point of  $k$  is lower than the  
5 apparent open-circuit voltage  $V'_o(k)$ , wherein  $V_o(k) = \Delta V_o(k) + V_{ini}$ , wherein  $V_o(k) = \Delta V_o(k)$ , when the calculated open-circuit voltage  $V_o(k)$  at the time point of  $k$  is lower than an apparent open-circuit voltage  $V'_o(k)$ .

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7. An estimating apparatus for a secondary cell as claimed in claim 6, wherein the output enabling power estimating section estimates the output enabling power ( $P_{out}$ ) using the following equation:

$$\left. \begin{aligned} P_{out} &= |I_{out\_max}| \cdot V_{min} \\ &= \frac{V_o - V_{min}}{e} \cdot V_{min} \end{aligned} \right]$$

15

, when the calculated open-circuit voltage  $V_o(k)$  at the time point of  $k$  is equal to or higher than the apparent open-circuit voltage  $V_o'(k)$  and

$$\begin{aligned}
 P_{out} &= |I_{out\_max}| \cdot V_{min} \\
 &= \frac{V_o - V_{min}}{e} \cdot V_{min} \\
 &= \frac{\frac{V_o}{b \cdot s + 1} - V_{min}}{e} \cdot V_{min}
 \end{aligned}
 \quad \boxed{\quad}$$

, when the calculated open-circuit voltage ( $V_o(k)$ ) at the time point of  $k$  is lower than the apparent open-circuit voltage ( $V'_o(k)$ ) at the time point of  $k$ .

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8. An estimating apparatus for a secondary cell as claimed in claim 7, wherein

$$\Delta V'_o = \frac{1}{T_3 \cdot s + 1} \cdot \Delta V_o \approx \frac{1}{b \cdot s + 1} \cdot \Delta V_o \text{ corresponds to } V_o/C(s) \text{ and}$$

$$\text{wherein } \Delta V_o = \frac{(T_1 \cdot s + 1)}{G_2(s)} \cdot V_o = a \cdot V_6 + b \cdot V_5 + V_4 - c \cdot I_6 - d \cdot I_5 - e \cdot I_4,$$

10 and wherein  $a = T_1 \cdot T_3$ ,  $b = T_1 + T_3$ ,  $c = K \cdot T_2 - T_3$ ,  $d = K \cdot (T_2 + T_3)$ ,  $e = K + h \cdot T_1 \approx K$ ,  $G_2(s)$  denotes a low pass filter,  $T_1$ ,  $T_2$ , and  $T_3$  denote each time constant, and

$$\begin{aligned}
 I_4 &= \frac{1}{G_2(s)} \cdot I & V_4 &= \frac{1}{G_2(s)} \cdot V \\
 I_5 &= \frac{s}{G_2(s)} \cdot I & V_5 &= \frac{s}{G_2(s)} \cdot V & \frac{1}{G_2(s)} &= \frac{1}{p_2 \cdot s + 1} \cdot \frac{1}{T_1 \cdot s + 1} \\
 I_6 &= \frac{s^2}{G_2(s)} \cdot I & V_6 &= \frac{s^2}{G_2(s)} \cdot V
 \end{aligned}
 \quad \boxed{\quad}$$

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9. An estimating apparatus for a secondary cell as claimed in claim 8, wherein the open-circuit voltage ( $V_o(k)$ ) at the time point of  $k$  is estimated from the following equation:

$$\frac{(T_1 \cdot s + 1)}{G_2(s)} \cdot V_0 = \frac{1}{G_2(s)}(a \cdot s^2 + b \cdot s + 1) \cdot V - \frac{1}{G_2(s)}(c \cdot s^2 + d \cdot s + K) \cdot I.$$

10. An estimating apparatus for a secondary cell  
as claimed in claim 9, wherein the parameter  
5 estimating section integrally estimates the  
parameters used in the equation (1) at one time as  
follows:

$$\theta = \begin{bmatrix} -a \\ -b \\ c \\ d \\ e \\ f \end{bmatrix}$$

wherein  $f = h$  and  $h$  denotes a variable efficiency  
10 derived from the following equation:  $V_0 = \frac{h}{s} \cdot I$ .

11. An estimating apparatus for a secondary cell  
as claimed in claim 10, wherein the equation (1) is  
arranged in an equivalent circuit model expressed as:

$$15 \quad V = \frac{K \cdot (T_2 \cdot s + 1)}{T_1 \cdot s + 1} \cdot I + \frac{1}{T_3 \cdot s + 1} \cdot V_o.$$

12. An estimating apparatus for a secondary cell as  
claimed in claim 1, wherein the adaptive digital  
filter uses the cell model described in the equation  
20 (2) and the parameter estimating section integrally  
estimates all parameters ( $\theta$ ) in the equation (2) at  
one time.

13. An estimating apparatus for a secondary cell  
25 as claimed in claim 12, wherein, in a case where the  
terminal voltage of the secondary cell immediately

before the secondary cell becomes a predetermined excessive charge is assumed to be a maximum enabling voltage ( $V_{max}$ ) and the terminal voltage of the secondary cell immediately before the secondary cell  
5 becomes a predetermined excessive discharge is assumed to be a minimum enabling voltage ( $V_{min}$ ), the input enabling power estimating section estimates the input enabling power ( $P_{in}$ ) of the secondary cell on the basis of the parameter estimated values ( $\theta$ ) and  
10 the open-circuit voltage ( $V_o$ ), and the maximum enabling voltage ( $V_{max}$ ) and the output enabling power estimating section estimates the output enabling power ( $P_{out}$ ) of the secondary cell on the basis of the parameter estimated values ( $\theta$ ), the open-circuit  
15 voltage ( $V_o$ ), and the minimum enabling voltage ( $V_{min}$ ).

14. An estimating apparatus for a secondary cell as claimed in claim 13, wherein the input enabling power estimating section estimates the input enabling power ( $P_{in}$ ) using the following equation:

$$P_{in} = I_{in\_max} \cdot V_{max} \\ = \frac{V_{max} - V_o}{K} \cdot V_{max}$$

, wherein  $I_{in\_max}$  denotes a maximum input current calculated from an equation:  $V = K \cdot I + V_o$ , wherein  $V_{max}$  is substituted for  $V$  and  $K$  denotes an internal resistance of the secondary cell which corresponds to one of the parameter estimated values ( $\theta$ ), and  $I_{in\_max}$  is substituted for  $I$ .

15. An estimating apparatus for a secondary cell  
30 as claimed in claim 14, wherein the output enabling

power estimating section estimates the output enabling power ( $P_{out}$ ) as follows:

$$\begin{aligned} P_{out} &= |I_{out\_max}| \cdot V_{min} \\ &= \frac{V_0 - V_{min}}{K} \cdot V_{min} \end{aligned} \quad ]$$

, wherein  $I_{out\_max}$  is a maximum output current  
5 calculated from an equation:  $V = K \cdot I + V_0$  in which  $V_{min}$  is substituted for  $V$  and  $I_{out\_max}$  is substituted for  $I$ .

16. An estimating apparatus for a secondary cell  
10 as claimed in claim 15, wherein the open-circuit voltage calculating section calculates the open-circuit voltage estimated value ( $V_0(k)$ ) at a time point of  $k$  as follows:  $V_0(k) = \Delta V_0(k) + V_{ini}$ , wherein  $V_{ini}$  denotes an initial value of the terminal voltage  
15 when no current is caused to flow into the secondary cell and  $\Delta V_0(k) = \Delta V_0 = G_{lp}(s) \cdot V_0 = V_1 + T_1 \cdot V_2 - K \cdot T_2 \cdot I_2 - K \cdot I_1$ ,  
wherein

$$\begin{aligned} G_{lp}(s) &= \frac{1}{(p \cdot s + 1)^3}, \quad V_2 = s \cdot G_{lp}(s) \cdot V, \quad V_1 = G_{lp}(s) \cdot V \\ &\quad I_2 = s \cdot G_{lp}(s) \cdot I, \quad I_1 = G_{lp}(s) \cdot I \end{aligned} \quad ]$$

, wherein  $G_{lp}(s)$  denotes a low pass filter,  $p$  denotes  
20 a constant determining a response characteristic of  $G_{lp}(s)$ , and  $T_1$  and  $T_2$  denote time constants of an equivalent circuit model of the secondary cell expressed in the equation (2).

25 17. An estimating apparatus for a secondary cell as claimed in claim 16, wherein the parameter estimating section integrally estimates all parameters used in the equation (2) at one time as follows:

$$\theta = \begin{bmatrix} -T_1 \\ K \cdot T_2 \\ K \\ h \end{bmatrix}$$

, wherein  $h$  denotes a variable efficiency and is derived from the following equation:  $V_o = \frac{h}{s} \cdot I$ .

5 18. An estimating apparatus for a secondary cell as claimed in claim 16, wherein, in the equation (2), when  $(T_1 \cdot s + 1)$  is substituted for  $A(s)$  and  $K \cdot (T_2 \cdot s + 1)$  is substituted for  $B(s)$ , the following equation is established:

10 
$$V = \frac{K \cdot (T_2 \cdot s + 1)}{T_1 \cdot s + 1} \cdot I + \frac{1}{T_1 \cdot s + 1} \cdot V_o.$$

19. An estimating apparatus for a secondary cell, comprising:

current detecting means for detecting a current  
15 (I) charged into and discharged from the secondary cell;

voltage detecting means for detecting a terminal voltage (V) across the secondary cell;

parameter estimating means for integrally  
20 estimating all parameters ( $\theta$ ) at one time in at least one of the following equations (1) and (2) with the measured current (I) and terminal voltage (V) inputted into an adaptive digital filter using a cell model described in a corresponding one of the following equations (1) and (2) whose parameters are estimated;

open-circuit voltage calculating means for calculating an open-circuit voltage ( $V_o$ ) using the

current (I), the terminal voltage (V), and the parameter estimated values ( $\theta$ );

input enabling power estimating means for estimating an input enabling power ( $P_{in}$ ) of the 5 secondary cell on the basis of the parameter estimated values ( $\theta$ ) and open-circuit voltage ( $V_o$ ); and

output power enabling power estimating means for estimating an output enabling power ( $P_{out}$ ) of the 10 secondary cell on the basis of the parameter estimated values and the open-circuit voltage ( $V_o$ ), the equation (1) being

$$V = \frac{B(s)}{A(s)} \cdot I + \frac{1}{C(s)} \cdot V_o \quad \dots (1), \text{ wherein}$$

$$A(s) = \sum_{k=0}^n a_k \cdot s^k, \quad B(s) = \sum_{k=0}^n b_k \cdot s^k, \quad C(s) = \sum_{k=0}^n c_k \cdot s^k, \quad s$$

15 denotes a Laplace transform operator,  $A(s)$ ,  $B(s)$ , and  $C(s)$  denote each poly-nominal of  $s$  ( $n$  denotes degrees),  $a_1 \neq 0$ ,  $b_1 \neq 0$ , and  $c_1 \neq 0$  and the equation

$$(2) \text{ being } V = \frac{B(s)}{A(s)} \cdot I + \frac{1}{A(s)} \cdot V_o \quad \dots (2), \text{ wherein}$$

$$A(s) = \sum_{k=0}^n a_k \cdot s^k \quad \text{and} \quad B(s) = \sum_{k=0}^n b_k \cdot s^k.$$

20

20. An estimating method for a secondary cell, comprising:

detecting a current (I) charged into and discharged from the secondary cell;

25 detecting a terminal voltage (V) across the secondary cell;

integrally estimating all parameters ( $\theta$ ) at one time in at least one of the following equations (1)

and (2) with the measured current ( $I$ ) and terminal voltage ( $V$ ) inputted into an adaptive digital filter using a cell model described in a corresponding one of the following equations (1) and (2) whose parameters are estimated;

5 calculating an open-circuit voltage ( $V_o$ ) using the current ( $I$ ), the terminal voltage ( $V$ ), and the parameter estimated values ( $\theta$ );

10 estimating an input enabling power ( $P_{in}$ ) of the secondary cell on the basis of the parameter estimated values ( $\theta$ ) and open-circuit voltage ( $V_o$ ); and

15 estimating an output enabling power ( $P_{out}$ ) of the secondary cell on the basis of the parameter estimated values and the open-circuit voltage ( $V_o$ ), the equation (1) being

$$V = \frac{B(s)}{A(s)} \cdot I + \frac{1}{C(s)} \cdot V_o \quad \dots (1), \text{ wherein}$$

$$A(s) = \sum_{k=0}^n a_k \cdot s^k, \quad B(s) = \sum_{k=0}^n b_k \cdot s^k, \quad C(s) = \sum_{k=0}^n c_k \cdot s^k, \quad s$$

denotes a Laplace transform operator,  $A(s)$ ,  $B(s)$ , and  $C(s)$  denote each poly-nominal of  $s$  ( $n$  denotes degrees),  $a_1 \neq 0$ ,  $b_1 \neq 0$ , and  $c_1 \neq 0$  and the equation

$$(2) \text{ being } V = \frac{B(s)}{A(s)} \cdot I + \frac{1}{A(s)} \cdot V_o \quad \dots (2), \text{ wherein}$$

$$A(s) = \sum_{k=0}^n a_k \cdot s^k \quad \text{and} \quad B(s) = \sum_{k=0}^n b_k \cdot s^k.$$